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# Numerical integration of the three-dimensional Green kernel for an electromagnetic problem $\stackrel{\text{\tiny{thet}}}{=}$

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# Abstract

In this paper, we present a method for the numerical integration of the three-dimensional Green kernel over two triangles. This method is compared with the results obtained by other algorithms. The comparison proves the efficiency of the technique in removing the numerical singularity. Furthermore, we provide a numerical algorithm for increasing the computation accuracy without refining the finite element mesh. © 2004 Elsevier Inc. All rights reserved.

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# 1. Introduction

This section presents the motivation for integrating the Green Kernel in order to solve an electromagnetic problem in a three-dimensional case. One of the possible applications of the problem is induction heating modeling. Rather than presenting the complete model, which can be found in various papers (see e.g., [1,2,4,5,12-14]), we will focus on the aspects that lead to the integrals we would like to calculate with precision.

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# 1.1. An electromagnetic model for induction heating

Induction heating is used for the thermal treatment of metal pieces in many industrial processes such as brazing, hardening or forging. Inductors in which are flowing alternating currents create a magnetic field which generates eddy currents in the pieces to be treated. The diffusion of the heat due to these currents makes possible the heating process.

Such a problem requires to solve a three-dimensional electromagnetic problem which has been worked out in [1,2,4,12–14]. This model is based on a description of the electromagnetic phenomena inside the conducting pieces and on their borders. The principle of this method consists in taking as unknowns the magnetic field in the conductors and the scalar magnetic potential on the edges of the conductors.

In that model, a so called device for induction heating consists in one or several inductors (current loops) and one or several conductors to be heated (workpieces).

Fig. 1 shows a description of such a system where the inductor is denoted by  $\Omega_i$  and the conductor by  $\Omega_i$ . The union of these two open domains is denoted by  $\Omega$ . The boundary of  $\Omega$  is  $\Gamma$  ( $\Gamma = \partial \Omega$ ) and the exterior of  $\Omega$  is  $\Omega_c$  ( $\Omega_c = \mathbb{R}^3 \setminus \overline{\Omega}$ ). The model requires to introduce two cuts  $S_i$  and  $\Sigma_i$  in  $\Omega_i$  as shown by Fig. 2. The cut  $S_i$  has a physical meaning and models the voltage supply, whereas the cut  $\Sigma_i$  appears for theoretical reasons (see [1,2,4,12–14]). Considering the geometry in Fig. 1, we make the following assumptions:

- The frequency of the generator being low enough, we neglect current displacements in Maxwell's equations.
- The various electromagnetic quantities will be written in their time-harmonic form.

With these approximations, Ampère's theorem, Faraday's law and Ohm's law enable writing the following system:

$$\begin{cases} \operatorname{curl} \vec{e} + \mathrm{i}\omega\mu\vec{h} = \vec{0} & \text{in } \mathbb{R}^3 \setminus S_i, \\ \operatorname{curl} \vec{h} = \sigma\vec{e} & \text{in } \Omega, \\ \operatorname{curl} \vec{h} = \vec{0} & \text{in } \Omega_c, \\ [\vec{e} \times \vec{n}]_{\Gamma} = [\vec{h} \times \vec{n}]_{\Gamma} = \vec{0} & \text{on } \Gamma, \end{cases}$$
(1)

where  $\vec{e}$ ,  $\vec{h}$  are, respectively, the electrical and the magnetic field. The quantity  $\sigma$  represents the electrical conductivity and  $\mu$  the magnetic permeability of materials,  $\omega$  is the angular frequency of the current. i is



Fig. 1. A device for induction heating.



Fig. 2. A model for the inductor.

the imaginary unit number.  $[f]_{\Gamma}$  is the jump of the quantity f on the interface  $\Gamma$ ,  $\vec{n}$  is the external normal vector to  $\Gamma$ . All the fields are complex valued.

In order to complete this system, we have to add a relation providing the harmonic voltage supply, V, applied to the inductor. This voltage is assumed to be given. We have:

$$\int_{c} (\vec{e} + i\omega\vec{a}) \cdot \vec{\tau} dc = V, \tag{2}$$

where  $\vec{a}$  is the vector potential defined by  $\vec{b} = \mu \vec{h} = \text{curl } \vec{a}$  and  $\text{div } \vec{a} = 0$  in  $\mathbb{R}^3$ , c is an oriented closed curve in  $\Omega_i$ , and  $\vec{\tau}$  is the unit tangent vector along c.

The system (1) and the Eq. (2) yield the equations to be solved so as to obtain the magnetic field in whole  $\mathbb{R}^3$ .

#### 1.2. The boundary element method

From Maxwell's equations, a variational formulation of the problem is written in  $\Omega \setminus S_i$ . After some manipulation, this variational formulation leads in particular to the computation of an integral over  $\Omega_c$ . Noticing that  $\vec{h}$  is vanishing Laplacian in  $\Omega_c$ , this integral can be decomposed into integrals on the boundary  $\Gamma$  involving the Steklov–Poincaré operator, also known as the Dirichlet–Neumann operator. This idea has been developed in [1] for electromagnetism.

The Steklov–Poincaré operator may be represented in function of two integro-differential operators: the so called simple and double layer potentials. The calculation of these potential yields integrals involving the Green kernel and its normal derivative.

Once the variational formulation has been obtained in the conductors and their edges, one uses a finite element technique to discretize the problem in space. We use a  $\mathbb{H}$  (**curl**) [12] finite element method to calculate the magnetic field in  $\Omega$  and a  $\mathbb{P}1$  finite element method to calculate on  $\Gamma$  the potential from which derives the magnetic field. A tetrahedral mesh is used, thus the triangulation of the edges is generated by the trace of the tetrahedrons on them. This method requires the numerical computation of the two integrals involving the Green kernel or its normal derivative over two edge triangles of the mesh. These two triangles may belong either to the same domain or to different ones.

These integrals correspond from the physical point of view to mutual inductances between the different parts of the system. They have their origin in the Biot–Savart law. This law reveals the Green kernel and allows the calculation of the magnetic scalar potential. We present in the next section these two integrals.

#### 1.3. The Green kernel integrals

Our aim is to provide an efficient method for calculating numerically the following integrals,

$$\int_{T_y} \int_{T_x} G(\vec{x}, \vec{y}) \,\mathrm{d}\Gamma_x \,\mathrm{d}\Gamma_y, \tag{3a}$$

$$\int_{T_y} q^k(\vec{y}) \int_{T_x} \frac{\partial G(\vec{x}, \vec{y})}{\partial n_x} \, \mathrm{d}\Gamma_x \, \mathrm{d}\Gamma_y, \tag{3b}$$

where  $G(\vec{x}, \vec{y})$  is the three-dimensional Green kernel defined by  $G(\vec{x}, \vec{y}) = -\frac{1}{4\pi} \frac{1}{\|\vec{x}-\vec{y}\|}$ ,  $\|.\|$  being the classical euclidean norm, and  $T_x$ ,  $T_y$  are two triangles of  $\mathbb{R}^3$ . The function  $q^k(\vec{y})$ , k = 0, 1, 2 is the  $\mathbb{P}1$  basis function at the node k of the triangle  $T_y$ . The normal vector  $\vec{n}_x$  is the unitary normal vector to the triangle  $T_x$ , external to the conductor to which  $T_x$  belongs. These two integrals are known to be convergent although the integrands are singular. When the two triangles  $T_x$ ,  $T_y$  are far enough from each other, a Gauss–Hammer integration rule provides good results [8]. Nevertheless, when the triangles grow closer and closer (but still distinct), the singularity of the integrands manifests itself and makes the numerical integration blow up. Such a phenomenon has been observed in the case of the numerical simulation of induction heating where the inductor surrounding the workpiece was near the latter. In practice we will be interested in calculating the integrals:

$$I_1 = \int_{T_y} \int_{T_x} \frac{1}{\|\vec{x} - \vec{y}\|} \, \mathrm{d}\Gamma_x \, \mathrm{d}\Gamma_y,\tag{4}$$

and

$$I_{2}^{k} = \int_{T_{y}} q^{k}(\vec{y}) \int_{T_{x}} \frac{(\vec{x} - \vec{y}) \cdot \vec{n}_{x}}{\|\vec{x} - \vec{y}\|^{3}} \, \mathrm{d}\Gamma_{x} \, \mathrm{d}\Gamma_{y}.$$
(5)

It is possible to find various approaches, for instance in [3,9,10], dealing with the numerical integration of a singular kernel over a triangle. However, most of them are not based upon exact integration for removing the singularity. An exact integration method has been developed in [7] and used in [6] in another physical context. This method is using Gauss integral theorems to transform the integration on a given triangle into one integration over the boundary of that triangle. We present here an alternative approach based on finding primitives, which leads to faster computations, as our comparisons will show it, and also to an exact formula in the specific but very important case where the two triangles of integration are overlapped.

# 2. Reduction of the integration over the reference triangle

#### 2.1. Variable transformation

In order to perform the calculation we introduce the variable transformation  $u_x$  that transforms the triangle  $T_x$  into the reference triangle,  $\hat{T}$ , whose nodes  $A_0$ ,  $A_1$ ,  $A_2$  have the coordinates (0,0), (0,1), (1,0) in the plane of the new variables ( $\xi_1$ ,  $\eta_1$ ). To define  $u_x$ , let's consider the following application: A. Masserey et al. | Journal of Computational Physics 205 (2005) 48-71

$$U_x: \quad \hat{T} \to T_x (\xi_1, \eta_1) \mapsto U_x(\xi_1, \eta_1) = \sum_{j=0}^2 u^j(\xi_1, \eta_1) \overrightarrow{OA_j},$$
(6)

where

$$\begin{cases} u^{0}(\xi_{1},\eta_{1}) = 1 - \xi_{1} - \eta_{1}, \\ u^{1}(\xi_{1},\eta_{1}) = \xi_{1}, \\ u^{2}(\xi_{1},\eta_{1}) = \eta_{1}. \end{cases}$$
(7)

and  $\overrightarrow{OA_j}$  is the vector with origin O, the arbitrary origin of  $\mathbb{R}^3$ , and extremity  $A_j$ . Then,  $u_x = U_x^{-1}$ . In the same way, we define the transformation,  $u_y$  that transforms the triangle  $T_y$  with nodes  $B_0$ ,  $B_1$ ,  $B_2$  into the reference triangle  $\hat{T}$  in the plane of the new variables  $(\xi_2, \eta_2)$ , as shown in Fig. 3. In our case we have to calculate an integral of the form,

$$I = \int_{T_y} \int_{T_x} F(\vec{x}, \vec{y}) \,\mathrm{d}\Gamma_x \,\mathrm{d}\Gamma_y,\tag{8}$$

where  $F(\vec{x},\vec{y})$  is a locally singular integrand for  $\vec{x} = \vec{y}$ . Thus,  $F(\vec{x},\vec{y})$  is known to be nonsingular when the triangles over which the integration is done are distinct and the integral to be calculated is well defined. However, when  $T_x$  and  $T_y$  have a non void intersection a numerical singularity appears. If  $T_x$  is very close to  $T_y$ , then the integrands in (3) are almost singular and numerical integration fails. By making the variable transformations  $u_x$  and  $u_y$  and defining  $f(\xi_1,\eta_1,\xi_2,\eta_2) = F(\vec{x},\vec{y})$ , with  $\vec{x} = U_x(\xi_1,\eta_1)$  and  $\vec{y} = U_y(\xi_2,\eta_2)$ , the integral *I* becomes:

$$I = 4|T_x||T_y| \int_{\hat{T}} \int_{\hat{T}} f(\xi_1, \eta_1, \xi_2, \eta_2) \, \mathrm{d}\xi_1 \, \mathrm{d}\eta_1 \, \mathrm{d}\xi_2 \, \mathrm{d}\eta_2, \tag{9}$$

where |T| is the measure of a given triangle T.

# 2.2. Numerical calculation of I

A pure numerical calculation of I may be done when  $T_x \cap T_y = \emptyset$  by using a N points Gauss–Hammer quadrature formula (see [1]):



Fig. 3. The transformations  $u_x$  and  $u_y$ .

A. Masserey et al. | Journal of Computational Physics 205 (2005) 48-71

$$I \approx 4|T_x||T_y| \sum_{i=1}^N \sum_{j=1}^N w_i w_j f(\xi^i, \eta^i, \xi^j, \eta^j),$$
(10)

where  $(\xi^i, \eta^i)$ , are the coordinates of the Gauss-Hammer's points belonging to  $\hat{T}$  and  $w_i$ , i = 1, ..., N, are the associated weights. However, when  $T_x \cap T_y \neq \emptyset$  or  $T_x \cap T_y = \emptyset$  with  $T_x$  very close to  $T_y$ , this formula leads to difficulties and we suggest another approach to compute *I*. Let us notice *I* may be rewritten as:

$$I = 4|T_x||T_y| \int_{\hat{T}} k(\xi_2, \eta_2) \,\mathrm{d}\xi_2 \,\mathrm{d}\eta_2, \tag{11}$$

where

$$k(\xi_2,\eta_2) = \int_0^1 \int_0^{1-\eta_1} f(\xi_1,\eta_1,\xi_2,\eta_2) \,\mathrm{d}\xi_1 \,\mathrm{d}\eta_1,\tag{12}$$

and

$$f(\xi_1,\eta_1,\xi_2,\eta_2) = \frac{1}{\|U_x(\xi_1,\eta_1) - U_y(\xi_2,\eta_2)\|},$$
(13)

or

$$f(\xi_1,\eta_1,\xi_2,\eta_2) = \frac{(U_x(\xi_1,\eta_1) - U_y(\xi_2,\eta_2)) \cdot \vec{n}_x}{\|U_x(\xi_1,\eta_1) - U_y(\xi_2,\eta_2)\|^3} q^k(\xi_2,\eta_2).$$
(14)

The idea is then to calculate exactly  $k(\xi_2, \eta_2)$  and to approximate *I* by a *N*-points Gauss–Hammer quadrature formula:

$$I \approx 4|T_{x}||T_{y}| \sum_{i=1}^{N} w_{i}k(\xi^{i}, \eta^{i}).$$
(15)

We will call this method a semi-analytic Gauss–Hammer integration with N points.We show in the following section how  $k(\xi_2, \eta_2)$  can be computed as well in the case of  $I_1$  as in the case of  $I_2^k$ ,  $k \in \{0,1,2\}$  (see (4) and (5)).

#### **3.** Calculation of $k(\xi_2, \eta_2)$

We now calculate the integral (12) exactly by finding primitives of the kernels defined by (4) and (5) after the reduction to the canonical triangle. Finding these primitives with a software such as Maple is not straightforward. In fact, several cases occur depending on the relative position of the triangles. The properties given here will allow us to identify these different cases and to check that the formulas we will obtain are well defined.

#### 3.1. Some useful properties

We will denote by  $\|\cdot\|$  the euclidean norm and by  $\overline{AB}$  the distance between two points A and B. We have for any arbitrary origin O and for  $M_x \in T_x$ ,  $M_y \in T_y$ :

$$\frac{1}{\|\vec{x} - \vec{y}\|} = \frac{1}{\overline{M_x M_y}} = \frac{1}{\sqrt{(\overline{OM_y} - \overline{OM_x}) \cdot (\overline{OM_y} - \overline{OM_x})}},$$
(16)

A. Masserey et al. | Journal of Computational Physics 205 (2005) 48-71

$$\frac{\left(\vec{x}-\vec{y}\right)\cdot\vec{n}_{x}}{\left\|\vec{x}-\vec{y}\right\|^{3}} = \frac{\left(\vec{x}-\vec{y}\right)\cdot\vec{n}_{x}}{\overline{M_{x}M_{y}}^{3}} = \frac{\left(\overrightarrow{OM_{x}}-\overrightarrow{OM_{y}}\right).\vec{n}_{x}}{\left[\left(\overrightarrow{OM_{y}}-\overrightarrow{OM_{x}}\right)\cdot\left(\overrightarrow{OM_{y}}-\overrightarrow{OM_{x}}\right)\right]^{\frac{3}{2}}},\tag{17}$$

where  $\vec{x} = \overrightarrow{OM_x}$  and  $\vec{y} = \overrightarrow{OM_y}$ . We also have:

$$\vec{x} = \overrightarrow{OA_0} + \xi_1 \overrightarrow{A_0A_1} + \eta_1 \overrightarrow{A_0A_2},\tag{18}$$

$$\vec{y} = \overrightarrow{OB_0} + \xi_2 \overrightarrow{B_0B_1} + \eta_2 \overrightarrow{B_0B_2}.$$
(19)

Defining the following variables:

$$\begin{cases} \beta = \overline{M_{y}A_{0}} \cdot \vec{n}_{x}, \\ d = \overline{A_{0}A_{1}}^{2}, \\ e = 2\overline{A_{0}A_{1}} \cdot \overline{M_{y}A_{0}}, \\ g = 2\overline{A_{0}A_{2}} \cdot \overline{A_{0}A_{1}}, \\ h = \overline{M_{y}A_{0}}^{2}, \\ j = 2\overline{A_{0}A_{2}} \cdot \overline{M_{y}A_{0}}, \\ k = \overline{A_{0}A_{2}}^{2}, \end{cases}$$
(20)

the squared distance  $\overline{M_x M_y}^2$  and the scalar product  $(\vec{x} - \vec{y}) \cdot \vec{n}_x$  may be written in function of the variables  $\xi_1, \eta_1$  as:

$$\overline{M_x M_y}^2 = \mathrm{d}\xi_1^2 + e\xi_1 + g\xi_1 \eta_1 + h + j\eta_1 + k\eta_1^2, \tag{21}$$

$$(\vec{x} - \vec{y}) \cdot \vec{n}_x = \beta. \tag{22}$$

We may then write the five following properties. Most of them are obvious and can be obtained through simple geometrical considerations.

Property 1:

$$j^{2} - 4kh = 4\overline{A_{0}A_{2}}^{2}\overline{M_{y}A_{0}}^{2} \left[\cos^{2}\left(\left(\overline{A_{0}A_{2}}, \overline{M_{y}A_{0}}\right)\right) - 1\right] \leqslant 0.$$

$$(23)$$

Property 2:

$$(j+g-e-2d)^{2} - 4(d+k-g)(d+h+e) = 4\overline{A_{1}A_{2}}^{2}\overline{M_{y}A_{1}}^{2} \Big[\cos^{2}((\overline{A_{1}A_{2}}, \overline{M_{y}A_{1}})) - 1\Big] \leqslant 0.$$
(24)

Property 3:

$$g \pm 2\sqrt{dk} = 2\overline{A_0A_1A_0A_2} \left[\cos^2(\overline{A_0A_1}, \overline{A_0A_2}) \pm 1\right] \neq 0,$$
(25)

because the points  $A_0$ ,  $A_1$ ,  $A_2$  are not aligned. Property 4:

$$(g-2d) \pm 2\sqrt{d(d+k-g)} = 2\overline{A_0A_1} \left[ \overline{A_0A_2} \cos(\overline{A_0A_1}, \overline{A_0A_2}) - \overline{A_0A_1} \pm \overline{A_1A_2} \right] \neq 0,$$
(26)

because the points  $A_0$ ,  $A_1$ ,  $A_2$  are not aligned.

Property 5:

$$(2eg - 4dj)^{2} - 4(g^{2} - 4dk)(e^{2} - 4dh)$$

$$= -64\overline{A_{0}A_{1}}^{4}\overline{A_{0}A_{2}}^{2}\overline{M_{y}A_{0}}^{2}\left[\sin^{2}(\overrightarrow{A_{0}A_{2}}, \overrightarrow{A_{0}A_{1}})\sin^{2}(\overrightarrow{A_{0}A_{1}}, \overrightarrow{M_{y}A_{0}})\sin^{2}(\widehat{A}_{1})\right] \leq 0, \qquad (27)$$

where  $\hat{A}_1$  is the dihedral angle between the two planes defined respectively by the points  $A_0$ ,  $A_1$ ,  $A_2$  and  $A_0$ ,  $A_1$ ,  $M_y$ . We get this equality by using the Gauss relations of the spherical trigonometry.

These five properties will be essential for the following sections.

# 3.2. Case $F(\vec{x}, \vec{y}) = \frac{1}{\|\vec{x} - \vec{y}\|}$

We have to distinguish between two situations. The first one is when the point  $M_y$  does not belong to the plane  $\mathscr{P}_x$  defined by the triangle  $T_x$ , the second when it belongs to  $\mathscr{P}_x$ .

# 3.2.1. $M_v$ does not belong to $\mathcal{P}_x$

The first integration over  $\xi_1$  corresponding to the relation (12) yields:

$$\int_{0}^{1-\eta_{1}} f(\xi_{1},\eta_{1},\xi_{2},\eta_{2}) d\xi_{1} = \frac{\ln((g-2d)\eta_{1}+e+2d+2\sqrt{\kappa(\eta_{1})}\sqrt{d}) - \ln(g\eta_{1}+e+2\sqrt{h+j\eta_{1}+k\eta_{1}^{2}}\sqrt{d})}{\sqrt{d}}$$

$$= \frac{\ln(\|\overline{A_{0}A_{1}}\|\|\overline{M_{y}A_{1}}+\eta_{1}\overline{A_{1}A_{2}}\| + \overline{A_{0}A_{1}} \cdot (\overline{M_{y}A_{1}}+\eta_{1}\overline{A_{1}A_{2}}))}{\overline{A_{0}A_{1}}}$$

$$- \frac{\ln(\|\overline{A_{0}A_{1}}\|\|\overline{M_{y}A_{0}}+\eta_{1}\overline{A_{0}A_{2}}\| + \overline{A_{0}A_{1}} \cdot (\overline{M_{y}A_{0}}+\eta_{1}\overline{A_{0}A_{2}}))}{\overline{A_{0}A_{1}}}$$
(28)

with

$$\kappa(\eta_1) = (h+d+e) + (j+g-e-2d)\eta_1 + (d+k-g)\eta_1^2.$$
<sup>(29)</sup>

We shall perform the second integration over  $\eta_1$  by using two variable changes. Under the assumption that  $M_y$  does not belong to  $\mathcal{P}_x$ , the arguments of the logarithms are always strictly positive for  $\eta_1 \in [0, 1]$ . Thus, we have to integrate over that interval two continuous functions of the form  $w(\eta_1) = \ln(A\eta_1 + B + K\sqrt{C\eta_1^2 + D\eta_1 + E})$ , where C is a positive number and where  $\Delta = D^2 - 4CE < 0$ , according to properties 1 and 2 with  $M_y$  not belonging to  $\mathcal{P}_x$ . We have:

$$w(\eta_1) = \ln\left(A\eta_1 + B + K\sqrt{C}\sqrt{\left(\eta_1 + \frac{D}{2C}\right)^2 - \frac{A}{4C^2}}\right).$$
(30)

Performing the first change of variable  $t = \eta_1 + \frac{D}{2C}$ , we obtain:

$$\int_{0}^{1} w(\eta_{1}) \,\mathrm{d}\eta_{1} = \int_{\frac{D}{2C}}^{1+\frac{D}{2C}} \ln\left(At - \frac{AD}{2C} + B + K\sqrt{C}\sqrt{t^{2} - \frac{A}{4C^{2}}}\right) \mathrm{d}t.$$
(31)

The second change of variable is  $t = \sqrt{-\frac{\Lambda}{4C^2}}\sinh(u)$ . Thus,

$$\int_{0}^{1} w(\eta_{1}) d\eta_{1} = \sqrt{-\frac{\Delta}{4C^{2}}} \int_{\operatorname{arcsinh}}^{\operatorname{arcsinh}} \left( \frac{1+D}{2C} \sqrt{-\frac{4C^{2}}{4}} \right) \\ \times \ln \left( A \sqrt{-\frac{\Delta}{4C^{2}}} \sinh(u) - \frac{AD}{2C} + B + K \sqrt{-\frac{\Delta}{4C}} \cosh(u) \right) \cosh(u) du.$$
(32)

We then have to integrate a function of the form  $\tilde{w}(u) = \ln(U\cosh(u) + V\sinh(u) + Z)\cosh(u)$ , where U, V, Z are real constants with respect to the integration. A primitive of such a function is given by:

$$\int \tilde{w}(u) \, du = \frac{\left(VZ - U\sqrt{Z^2 + V^2 - U^2}\right) \ln\left(e^u + \frac{\sqrt{Z^2 + V^2 - U^2 + Z}}{(V+U)}\right)}{V^2 - U^2} + \frac{\left(U\sqrt{Z^2 + V^2 - U^2} + VZ\right) \ln\left(e^u + \frac{-\sqrt{Z^2 + V^2 - U^2} + Z}{(V+U)}\right)}{V^2 - U^2} - \frac{Zu}{V - U} + \sinh(u)[\ln(U\cosh(u) + V\sinh(u) + Z) - 1].$$
(33)

According to properties 3 and 4, we may check that  $V \pm U \neq 0$ . Although this formula has to be used when  $M_y$  does not belong to  $\mathscr{P}_x$ , it works in the particular case where  $M_y$  belongs to  $\mathscr{P}_x$  and lies inside the triangle  $A_0$ ,  $A_1$ ,  $A_2$ , out of the edges. Then, the expression (28) is well defined (no logarithm of zero).

3.2.2.  $M_y$  belongs to  $\mathcal{P}_x$ 

Let us consider first the integrals

$$K_i(\vec{y}) = \int_{T_x^i} F(\vec{x}, \vec{y}) \,\mathrm{d}\Gamma_x, \quad K(\vec{y}) = \int_{T_x} F(\vec{x}, \vec{y}) \,\mathrm{d}\Gamma_x, \tag{34}$$

where the vertices of triangle  $T_x^i$  are the points  $M_y$ ,  $A_i$ ,  $A_{i+1}$ ,  $i \in \{0, 1, 2\}$ , the sums being taken modulo 3. Performing the first change of variables defined by,  $\vec{x} = (1 - \xi_1 - \eta_1)\overrightarrow{OA_i} + \xi_1\overrightarrow{OM_y} + \eta_1\overrightarrow{OA_{i+1}}$ , we obtain

$$K_{i}(\vec{y}) = 2|T_{x}^{i}|nt_{\hat{T}}\frac{\mathrm{d}\xi_{1}\mathrm{d}\eta_{1}}{\|(1-\xi_{1})\vec{v}_{i}-\eta_{1}\vec{a}_{i}\|},\tag{35}$$

with  $\vec{v}_i = \overrightarrow{M_y A_i}$  and  $\vec{a}_i = \overrightarrow{A_{i+1} A_i}$ . Making then the second change of variables  $\xi_1 = s$ ,  $\eta_1 = (1-s)t$ , we get:

$$K_{i}(\vec{y}) = 2|T_{x}^{i}| \int_{0}^{1} \frac{\mathrm{d}t}{\|\vec{v}_{i} - t\vec{a}_{i}\|} = 2|T_{x}^{i}| \int_{0}^{1} \frac{\mathrm{d}t}{\sqrt{\|\vec{a}_{i}\|^{2}t^{2} - 2\vec{v}_{i}\cdot\vec{a}_{i}t + \|\vec{v}_{i}\|^{2}}}.$$
(36)

The calculation of that integral gives:

$$K_{i}(\vec{y}) = 2 \frac{|T_{x}^{i}|}{\|\vec{a}_{i}\|} (\ln\left((\vec{a}_{i} - \vec{v}_{i}) \cdot \vec{a}_{i} + \|\vec{a}_{i} - \vec{v}_{i}\|\|\vec{a}_{i}\|) - \ln\left(\|\vec{a}_{i}\|\|\vec{v}_{i}\| - \vec{v}_{i} \cdot \vec{a}_{i}\right)).$$
(37)

It is easy to check that this formula is always well defined under our assumptions provided that the triangle  $T_x^i$  is not degenerate. However, if it is the case  $|T_x^i| = 0$  and  $K_i(\vec{y}) = 0$ .

At that stage, we may notice that it is always possible to express the domain  $T_x$  as a combination of the domains  $T_x^0$ ,  $T_x^1$ ,  $T_x^2$  such that  $K(\vec{y}) = \epsilon_0 K_0(\vec{y}) + \epsilon_1 K_1(\vec{y}) + \epsilon_2 K_2(\vec{y})$ , where  $\epsilon_i = \pm 1$ ,  $i \in \{0,1,2\}$  an example is given by the Fig. 4.



Fig. 5. Value of I in function of  $I_i$ ,  $I_{i+1}$  and  $I_{i+2}$  depending on the region to which  $M_y$  belongs. At the interfaces, one or two integrals from  $I_i$ ,  $I_{i+1}$  and  $I_{i+2}$  vanish.

The values of the  $\epsilon_i$  are the same as in the unique combination from seven possible ones that gives the area of the triangle  $T_x$  in function of the measures of the triangles  $T_x^i$ , as shown by the Fig. 5:  $|T_x| = \epsilon_0 |T_x^0| + \epsilon_1 |T_x^1| + \epsilon_2 |T_x^2|.$ 

If we consider 
$$I_i = \int_{T_y}^{T_i} K_i(\vec{y}) d\Gamma_y$$
,  $I_i$  is numerically computed by  
 $I_i \approx 2|T_y| \sum_{j=1}^N w_j K_i(U_y(\xi_2^j, \eta_2^j)).$   
Then,  $I \approx \epsilon_0 I_0 + \epsilon_1 I_1 + \epsilon_2 I_2.$ 

3.2.3. The particular case when  $T_x$  and  $T_y$  are the same triangles

In that case, it is possible to obtain an exact formula for *I*. The point  $M_y$  belongs to the triangle  $T_x$  as shown by the Fig. 6 and we have  $I = \sum_{i=0}^{2} \int_{T_y} K_i(\vec{y}) d\Gamma_y$ . Using the relation (37), we split this integral in two parts:

$$I = \sum_{i=0}^{2} (E_2^i - E_1^i), \tag{38}$$



Fig. 6. Situation when  $T_x$  and  $T_y$  are the same.

with

$$E_{2}^{i} = \int_{T_{y}} 2 \frac{|T_{x}^{i}|}{\|\vec{a}_{i}\|} \ln\left((\vec{a}_{i} - \vec{v}_{i}) \cdot \vec{a}_{i} + \|\vec{a}_{i} - \vec{v}_{i}\|\|\vec{a}_{i}\|\right) \mathrm{d}\Gamma_{y},\tag{39}$$

and

$$E_{1}^{i} = \int_{T_{y}} 2\frac{|T_{x}^{i}|}{\|\vec{a}_{i}\|} \ln\left(\|\vec{a}_{i}\|\|\vec{v}_{i}\| - \vec{v}_{i} \cdot \vec{a}_{i}\right) \mathrm{d}\Gamma_{y}.$$
(40)

Where we consider  $E_2^i$ , we perform successively the two changes of variables defined by:  $\vec{y} = (1 - \xi_1 - \eta_1) \overrightarrow{OA_i} + \xi_1 \overrightarrow{OA_{i+1}} + \eta_1 \overrightarrow{OA_{i+2}}$  and  $\xi_1 = s$ ,  $\eta_1 = (1-s)t$ , which gives  $\vec{a}_i - \vec{v}_i = (1-s)(\vec{a}_i + t\vec{a}_{i+2})$ and  $2|T_x^i| = 2(1-s)t|T_x|$ . We obtain:

$$E_{2}^{i} = 4 \frac{|T_{x}|^{2}}{\|\vec{a}_{i}\|} \int_{\tilde{T}} (1-s)^{2} t \ln(1-s) ((\vec{a}_{i}+t\vec{a}_{i+2}) \cdot \vec{a}_{i}+\|\vec{a}_{i}+t\vec{a}_{i+2}\|\|\vec{a}_{i}\|) \,\mathrm{d}s \,\mathrm{d}t, \tag{41}$$

where  $\tilde{T}$  is the unit square in the plane (s, t). The integration gives:

$$E_{2}^{i} = 4 \frac{|T_{x}|^{2}}{\|\vec{a}_{i}\|} \left( -\frac{5}{36} + \frac{\|\vec{a}_{i}\|(\|\vec{a}_{i+1}\| - \|\vec{a}_{i}\|)}{6\|\vec{a}_{i+2}\|^{2}} + \frac{1}{6} \ln(\|\vec{a}_{i+1}\| \|\vec{a}_{i}\| + \|\vec{a}_{i}\|^{2} + \vec{a}_{i} \cdot \vec{a}_{i+2}) + \frac{\|\vec{a}_{i}\|\|\vec{a}_{i}\cdot\vec{a}_{i+2}}{6\|\vec{a}_{i}\|^{3}} \ln\left( \frac{\|\vec{a}_{i}\|\|\vec{a}_{i+2}\| + \vec{a}_{i} \cdot \vec{a}_{i+2}}{\|\vec{a}_{i+2}\|^{2} + \vec{a}_{i} \cdot \vec{a}_{i+2}} \right) \right).$$

$$(42)$$

Where we consider  $E_1^i$ , we perform successively the two changes of variables defined by:  $\vec{y} = (1 - \xi_1 - \eta_1) \overrightarrow{OA_{i+1}} + \xi_1 \overrightarrow{OA_i} + \eta_1 \overrightarrow{OA_{i+2}}$  and  $\xi_1 = s$ ,  $\eta_1 = (1 - s)t$ , which gives  $\vec{v}_i = (1 - s)(\vec{a}_i + t\vec{a}_{i+1})$ and  $2|T_x^i| = 2(1 - s)t|T_x|$ . We obtain:

$$E_{1}^{i} = 4 \frac{|T_{x}|^{2}}{\|\vec{a}_{i}\|} \int_{\tilde{T}} (1-s)^{2} t \ln(1-s) (\|\vec{a}_{i}+t\vec{a}_{i+1}\| \|\vec{a}_{i}\| - (\vec{a}_{i}+t\vec{a}_{i+1}) \cdot \vec{a}_{i}) \,\mathrm{d}s \,\mathrm{d}t.$$
(43)

The integration gives:

$$E_{1}^{i} = 4 \frac{|T_{x}|^{2}}{\|\vec{a}_{i}\|} \left( -\frac{5}{36} + \frac{\|\vec{a}_{i}\|(\|\vec{a}_{i}\| - \|\vec{a}_{i+2}\|)}{6\|\vec{a}_{i+2}\|^{2}} + \frac{1}{6} \ln(\|\vec{a}_{i+2}\|\|\|\vec{a}_{i}\| - \|\vec{a}_{i}\|^{2} - \vec{a}_{i} \cdot \vec{a}_{i+1}) + \frac{\|\vec{a}_{i}\|\vec{a}_{i} \cdot \vec{a}_{i+1}}{6\|\vec{a}_{i+1}\|^{3}} \ln\left(\frac{\|\vec{a}_{i+1}\|\|\vec{a}_{i+2}\| + \|\vec{a}_{i+1}\|^{2} + \vec{a}_{i} \cdot \vec{a}_{i+1}}{\|\vec{a}_{i}\|\|\vec{a}_{i+1}\| + \vec{a}_{i} \cdot \vec{a}_{i+1}}\right) \right).$$

$$(44)$$

Summing over *i*, we get the final formula:

$$I = \frac{2}{3} |T_x|^2 \sum_{(i,j,k)\in\mathscr{F}} \left( \frac{n_i^2 - p_{ik}}{n_i^3} \ln(p_{ik} + n_i^2 + n_i n_j) - \frac{1}{n_i} \ln(-p_{ij} - n_i^2 + n_i n_k) + p_{jk} \left( \frac{1}{n_j^3} + \frac{1}{n_k^3} \right) \ln(p_{jk} + n_j n_k) - \frac{p_{ij}}{n_i^3} \ln(p_{ij} + n_i^2 + n_i n_k) \right),$$

$$(45)$$

where:  $\mathscr{F} = \{(0,1,2); (1,2,0); (2,0,1)\}, n_i = ||\vec{a}_i|| \text{ and } p_{ij} = \vec{a}_i \cdot \vec{a}_j.$ 

3.3. Case  $F(\vec{x}, \vec{y}) = \frac{(\vec{x} - \vec{y}).\vec{n}_x}{\|\vec{x} - \vec{y}\|^3} q^k(\vec{y})$ 

We have to calculate the integral:

$$\int_{0}^{1} \int_{0}^{1-\eta_{1}} f(\xi_{1},\eta_{1},\xi_{2},\eta_{2}) \,\mathrm{d}\xi_{1} \,\mathrm{d}\eta_{1} = \int_{0}^{1} \int_{0}^{1-\eta_{1}} \frac{\beta q^{k}(\xi_{2},\eta_{2})}{\left(\mathrm{d}\xi_{1}^{2} + e\xi_{1} + g\xi_{1}\eta_{1} + h + j\eta_{1} + k\eta_{1}^{2}\right)^{\frac{3}{2}}} \,\mathrm{d}\xi_{1} \,\mathrm{d}\eta_{1},\tag{46}$$

The function  $q^k(\xi_2, \eta_2)$  is constant with respect to  $(\xi_1, \eta_1)$ ; it is not restrictive to consider  $q^k = 1$ . Then, we split the integration in two parts such that:

$$\int_{0}^{1-\eta_{1}} \frac{\beta}{\left(d\xi_{1}^{2}+e\xi_{1}+g\xi_{1}\eta_{1}+h+j\eta_{1}+k\eta_{1}^{2}\right)^{\frac{3}{2}}} d\xi_{1} = Q_{1} + Q_{2},$$
(47)

where

$$Q_1 = 2 \frac{\beta(2d-g)\eta_1 - \beta(2d+e)}{z(\eta_1)\sqrt{(d+k-g)\eta_1^2 + (g+j-e-2d)\eta_1 + e+d+h}},$$
(48)

$$Q_2 = 2 \frac{\beta g \eta_1 + \beta e}{z(\eta_1) \sqrt{k \eta_1^2 + j \eta_1 + h}},$$
(49)

with

$$z(\eta_1) = \left(g^2 - 4dk\right)\eta_1^2 + \left(-4dj + 2eg\right)\eta_1 + e^2 - 4dh.$$
(50)

In order to perform the second integration we are led to find the integral of a function of the form:

$$w(\eta_1) = \frac{b\eta_1 + c}{(n\eta_1^2 + l\eta_1 + m)\sqrt{r\eta_1^2 + s\eta_1 + t}}.$$
(51)

We may consider a classification based upon several cases induced by the values of the quantities  $s^2 - 4rt$ , the discriminant of  $r\eta_1^2 + s\eta_1 + t$  and  $l^2 - 4nm$ , the discriminant of  $n\eta_1^2 + l\eta_1 + m$ , in relation with the properties 1, 2 and 5.

3.3.1. Case 1:  $s^2 - 4rt = 0$ 

When this case occurs, it means according to properties 1 and 2 that  $M_y$  belongs to the plane defined by the points  $A_0$ ,  $A_1$ ,  $A_2$ . Then, the coefficient  $\beta$  in (48) and (49) is zero and  $Q_1 = Q_2 = 0$ . Thus:

$$\int_{0}^{1} w(\eta_1) \, \mathrm{d}\eta_1 = 0. \tag{52}$$

# 3.3.2. Case 2: $s^2 - 4rt < 0$

In order to perform the exact integration in this case let us first explicit  $\zeta$  and  $\varsigma$ , the roots of the equation  $n\eta_1^2 + l\eta_1 + m = 0$ , and two other related quantities,  $\phi$  and  $\psi$ :

$$\zeta = \frac{-l - \sqrt{l^2 - 4nm}}{2n},\tag{53}$$

$$\varsigma = \frac{-l + \sqrt{l^2 - 4nm}}{2n},\tag{54}$$

$$\phi = \sqrt{2(r\varsigma^2 + s\varsigma + t)},\tag{55}$$

$$\psi = \sqrt{2(r\zeta^2 + s\zeta + t)}.$$
(56)

subcase 1:  $l^2 - 4nm = 0$ 

According to property 5, this means that  $M_y$  belongs to  $\mathcal{P}_x$ . Then, like previously, the coefficient  $\beta$  in (48) and (49) is equal to zero and  $Q_1 = Q_2 = 0$ . Thus:

$$\int_0^1 w(\eta_1) \, \mathrm{d}\eta_1 = 0. \tag{57}$$

subcase 2:  $l^2 - 4nm < 0$ ,  $\phi \neq 0$  and  $\psi \neq 0$ 

Then,  $\zeta$  and care the complex conjugated roots of  $n\eta_1^2 + l\eta_1 + m = 0$  but are not the roots of  $r\eta_1^2 + s\eta_1 + t = 0$ . Using Maple we get a primitive of w:

$$\int w(\eta_1) \, \mathrm{d}\eta_1 = \sqrt{2} \frac{\ln\left(\frac{\psi^2 + (s+2r\zeta)(\eta_1 - \zeta) + \sqrt{2}\psi\sqrt{r\eta_1^2 + s\eta_1 + t}}{\eta_1 - \zeta}\right)(b\zeta + c)}{n(\zeta - \zeta)\psi} - \sqrt{2} \frac{\ln\left(\frac{\phi^2 + (s+2r\zeta)(\eta_1 - \zeta) + \sqrt{2}\psi\sqrt{r\eta_1^2 + s\eta_1 + t}}{\eta_1 - \zeta}\right)(b\zeta + c)}{n(\zeta - \zeta)\phi}.$$
(58)

We may check under our assumptions that this expression is well defined (no divisions by zero) for  $\eta_1 \in [0, 1]$ . We have the difference of two complex quantities, which gives a real value after combining the conjugated expressions.

subcase 3:  $l^2 - 4nm < 0$ ,  $\phi = 0$  and  $\psi = 0$ 

The assumptions of the present subcase mean that  $\zeta$  and  $\zeta$  are not only the complex conjugated roots of  $n\eta_1^2 + l\eta_1 + m$ , but also the complex conjugated roots of  $r\eta_1^2 + s\eta_1 + t$ . Thus, the expression (51) has to be rewritten as:

$$w(\eta_1) = \frac{1}{n\sqrt{r}} \frac{b\eta_1 + c}{(\eta_1^2 - S\eta_1 + P)^{\frac{3}{2}}},$$
(59)

where  $S = \zeta + \overline{\zeta}$  and  $P = \zeta \overline{\zeta}$ . A primitive of w is then given by:

$$\int w(\eta_1) \,\mathrm{d}\eta_1 = \frac{2}{n\sqrt{r}} \frac{-(bS+2c)\eta_1 + cS + 2bP}{(S^2 - 4P)\sqrt{\eta_1^2 - S\eta_1 + P}}.$$
(60)

This formula is always well defined in that case because  $n \neq 0$ ,  $r \neq 0$  and  $S^2 - 4P < 0$ , which implies  $\eta_1^2 - S\eta_1 + P > 0$  for any  $\eta_1 \in [0, 1]$ .

## 3.4. Conclusion of this section

We were led to consider several cases in order to perform an exact integration to find  $k(\xi_2, \eta_2)$  for the computation of  $I_1$  and  $I_2^k$ . In each one we gave the formula to be used. These formulas have no more numerical singularities and may be integrated safely by a Gauss-Hammer quadrature rule.

#### 4. Comparisons between numerical and semi-analytic Gauss-Hammer integration

In this section, we make numerical experiments with the geometrical configuration presented by the Fig. 7. In that case the triangles  $T_x$  and  $T_y$  have the same shape and lie in two distinct parallel planes, one triangle over an other such that the distance between these two triangles may be defined as the distance between these planes. When the distance decreases to zero, the overlapping of the triangles becomes maximal so that the numerical singularities should be extreme. Let h be the distance between the two triangles and  $a_0$  be the parameter defined in the next section. We compare the calculation of the integrals of kind  $I_1$  and  $I_2^0$  versus the dimensionless variable  $h/a_0$  by different numerical methods and show the improvement obtained by the semi-analytical Gauss–Hammer integration in removing the numerical singularity. Details about the other numerical methods are available in references [8,11]. We also give calculation time cost comparisons.

#### 4.1. Comparisons between different numerical methods

We compare the following methods in order to compute numerically I of the relation (15): Gauss-Hammer quadrature formula with N = 3 points (GH<sub>3</sub>) and N = 9 points (GH<sub>9</sub>), adaptive double



Fig. 7. The configuration of  $T_x$  and  $T_y$  for numerical experiments.

exponential quadrature (ADEXP), semi-analytic Gauss–Hammer quadrature formula with N = 3 points (SAGH<sub>3</sub>) and N = 9 points (SAGH<sub>9</sub>), the exact integration method used in [6,7], based on boundary integration (EBI).

We chose as a reference for comparisons two methods: a method using the one-dimensional adaptive double exponential quadrature, because it is known to handle very well the kernels having local removable singularities (see for instance [11] for the double exponential transformation in numerical analysis), and EBI an alternative exact integration method from which we should get the same results. However, unlike in [6] where the numerical integration over the second triangle is done by the use of one-dimensional quadrature formulas, we combine the use of EBI with the two-dimensional Gauss–Hammer quadrature formulas with N = 9 points (EBI<sub>9</sub>) for the integration over that second triangle.

We apply the double exponential algorithm to the exact formula obtained by the first integration in (12), this formula still not removing the numerical singularities. We required ten digits of precision in order to compute this integral with accuracy, the second double integration being performed by a Gauss–Hammer rule with N = 9 points.

The results comparing all the methods except EBI<sub>9</sub> are presented on Fig. 8 for  $I_1$  and Fig. 9 for  $I_2^0$  (see (4) and (5) for the definition). In both cases the upper graph is a zoom of the lower one. Fig. 10 is devoted to the comparison between SAGH<sub>9</sub> and EBI<sub>9</sub> for the computation of  $I_0$  and  $I_2^0$ . For these comparisons the coordinates of the points corresponding to the corners of the two triangles are:  $A_0(-a,0,0)$ ,  $A_1(a,0,0)$ ,  $A_2(0,a,0)$ ,  $B_0(-a,0,h)$ ,  $B_1(a,0,h)$ ,  $B_2(0,a,h)$ . We took  $a = a_0 = 5 \times 10^{-3}$ . The dimensionless ratio  $h/a_0$  varies in the interval  $[2 \times 10^{-4}, 2]$ .

Figs. 8 and 9 show that the semi-analytical method does not blow up when  $h/a_0$  tends to zero and gives values in accordance with those obtained by the adaptive double exponential quadrature, whereas the pure numerical Gauss–Hammer method is diverging when  $h/a_0$  tends to zero. However, we can see that for the two kinds of integrals,  $I_1$  and  $I_2^0$ , the various methods give similar values when  $h/a_0$  is greater than 1, for that particular geometrical configuration.

In addition, it is possible to check that  $I_1$  converges to the value calculated by the exact formula for overlapped triangles, i.e.,  $I_1(0) = 3.5611 \times 10^{-7}$  when  $h/a_0$  tends to zero, and that  $I_2^0$  converges to zero when  $h/a_0$  tends to zero, as it is indicated by the the definition of this integral.

To compare SAGH<sub>9</sub> with EBI<sub>9</sub>, we implemented the formulas given in the appendix of [6]. Fig. 10 shows that the results obtained by SAGH<sub>9</sub> and EBI<sub>9</sub> are the same, as expected.

These two integrals are functions of the parameter *a* and the distance *h*, such that we may write  $I_1 = I_1(a,h)$  and  $I_2^0 = I_2^0(a,h)$ . If we want to deduce their values for any couple (a, h) from the values calculated with  $(a_0, h)$ , we may use the following properties:

$$\begin{cases} I_1(\lambda a,\lambda h) = \lambda^3 I_1(a,h), & I_1(\lambda a,h) = \lambda^3 I_1(a,\frac{h}{\lambda}), \\ I_2^0(\lambda a,\lambda h) = \lambda^2 I_2^0(a,h), & I_2^0(\lambda a,h) = \lambda^2 I_2^0(a,\frac{h}{\lambda}), \end{cases}$$
(61)

where  $\lambda$  is a strictly positive factor. Thus, if we want to know the values of these integrals for a given ratio h/a, we have to multiply the values given by Fig. 8 by the conversion factor  $\lambda$  to the power 3 and the values given by Fig. 9 by the conversion factor  $\lambda$  to the power 2.

Examining the time cost related with these two methods, we notice that the ratio between a Gauss–Hammer quadrature method with N = 3 points and N = 9 points is about 9, which corresponds to the ratio of the number of loops for computation between the two methods. The same thing holds for the semi-analytic Gauss–Hammer method.

The adaptive double exponential quadrature method ([11]) is very expensive in time, in particular because ten digits of precision were required in order to approximate with a good accuracy the exact value obtained for the integral over  $T_x$ .



Fig. 8. Comparisons between different numerical methods and relative associated time costs for  $I_1$ .



Fig. 9. Comparisons between different numerical methods and relative associated time costs for  $I_2^0$ .

Comparing the time costs between semi-analytic and pure Gauss–Hammer methods, we can see for  $I_2^0$ , with N = 9 points, the semi-analytic Gauss–Hammer method is 23% faster than a pure Gauss–Hammer method, whereas it is 40% slower in the case of  $I_1$ .



Fig. 10. Comparisons between SAGH<sub>9</sub> and EBI<sub>9</sub> for the computation of  $I_0$  and  $I_2^0$  and relative associated time costs.

Comparing now SAGH<sub>9</sub> with EBI<sub>9</sub>, we get that SAGH<sub>9</sub> is 3.4 times faster for the computation of  $I_0$  and 4.5 times faster for the computation of  $I_2^0$ . This can be explained by the differences between the formulas obtained in the two methods even if they give the same results.

The time cost of the semi-analytic Gauss–Hammer method is related to the complexity of the formula obtained by exact integration. However, the semi-analytic method reduces considerably the calculation time when the computation of the exact formula becomes faster than the computation of the nested sum of the pure numerical integration, which happens when the number of quadrature points is increased.

In practice, we would like to perform our computations using the fastest and the most accurate method. In a general configuration of the triangles, there are no exact formulas to compare with numerical calculations. However, the semi-analytical Gauss–Hammer quadrature method improves the computation error by removing the numerical singularity and cancelling one quadrature rule, with a computation time of the same order compared to the pure quadrature methods we tested. But this improvement may not be satisfactory. Thus, we present in the sequel a method allowing to obtain a better accuracy of the computation.

#### 5. Improvement of the computation accuracy

In the previous sections, we have shown how it was possible to remove the singularities in the numerical integrations by using partial exact integrations. After the exact integration there is still a pure numerical one to be computed. The resulting error is not known in the three-dimensional case unlike in the one-dimensional one where error estimations exist. Due to the lack of an exact formula enabling comparisons, except when the two integration triangles are the same, we are led to chose an algorithmic method for efficient computation. Inspired by the one-dimensional case, we have chosen to keep the number of Gauss–Hammer points constant. It is well known in the case of the numerical integration of a one-dimensional singular kernel that it is better to increase the number of integration intervals rather than the number of Gauss–Legendre points to achieve a given precision. Thus, the number of quadrature points was fixed to N = 9 and the integration triangle was subdivided into sub-triangles in a particular manner. We describe in this chapter this subdivision algorithm allowing to increase the precision. To show the efficiency of the method we make a comparison in the case where the two triangles of integration are the same for the integration of the Green kernel, the only case for which we have an exact formula.

#### 5.1. Decomposition of the integration by subdivision of the triangle T

We explain here how we subdivide the reference triangle to decompose the integration. Fig. 11 shows the subdivision method for the first step.

Let us consider the integration of a continuous function k over the reference triangle  $\hat{T}$ . If we denote by  $T_A$  the triangle determined by the points O(0,0), A(0,1),  $J(\frac{1}{2},\frac{1}{2})$  and by  $T_B$  the triangle determined by the points O(0,0), B(1,0),  $J(\frac{1}{2},\frac{1}{2})$ , we may write:

$$K = \int_{\hat{T}} k(\xi,\eta) \,\mathrm{d}\xi \,\mathrm{d}\eta = \int_{T_A} k(\xi,\eta) \,\mathrm{d}\xi \,\mathrm{d}\eta + \int_{T_B} k(\xi,\eta) \,\mathrm{d}\xi \,\mathrm{d}\eta.$$
(62)

Considering the mappings

$$U_A: T \to T_A$$
  

$$(\xi', \eta') \mapsto U_A(\xi', \eta') = Ju^0(\xi', \eta') + Au^2(\xi', \eta'),$$
(63)

and



Fig. 11. Transformations mapping the triangles  $T_A$  and  $T_B$  to  $\hat{T}$ .

$$U_B: \hat{T} \to T_B$$

$$(\xi', \eta') \mapsto U_B(\xi', \eta') = Ju^0(\xi', \eta') + Bu^2(\xi', \eta'),$$
(64)

inducing two variable transformations, we have:

$$\int_{T_A} k(\xi,\eta) \,\mathrm{d}\xi \,\mathrm{d}\eta = |\hat{T}| \int_{\hat{T}} k \circ U_A(\xi',\eta') \,\mathrm{d}\xi' \,\mathrm{d}\eta',\tag{65}$$

and

$$\int_{T_B} k(\xi,\eta) \,\mathrm{d}\xi \,\mathrm{d}\eta = |\hat{T}| \int_{\hat{T}} k \circ U_B(\xi',\eta') \,\mathrm{d}\xi' \,\mathrm{d}\eta'.$$
(66)

Then, the two integrals above, being defined over the reference triangle, may be integrated by a Gauss– Hammer quadrature formula applied to the functions  $k \circ U_A$  or  $k \circ U_B$ . The subdivision procedure may be continued until the wanted accuracy is reached. Thus, by iterating this process P times ( $P \ge 1$ ), we get

$$K = K_P = \left|\hat{T}\right|^P \sum_{\Pi \in \mathscr{A}_P} \int_{\hat{T}} k \circ U_{\Pi(1)} \circ U_{\Pi(2)} \cdots \circ U_{\Pi(P)}(\xi_P^{\Pi}, \eta_P^{\Pi}) \,\mathrm{d}\xi_P^{\Pi} \,\mathrm{d}\eta_P^{\Pi},\tag{67}$$

where  $\mathscr{A}_P$  is the set of mappings from the set  $\{1, \ldots, P\}$  to the set  $\{A, B\}$  and  $(\xi_n^\Pi, \eta_n^\Pi)_{n=1, \ldots, P}$  is the sequence of variables due to the variable transformations induced by a given  $\Pi \in \mathscr{A}_P$ . The relation between  $(\xi_n^\Pi, \eta_n^\Pi)$  and  $(\xi_{n+1}^\Pi, \eta_{n+1}^\Pi)$  can be derived by writing the mappings  $U_A$  and  $U_B$  in a matrix form. Let us define for that purpose the following quantities:

$$M_{A} = \frac{1}{2} \begin{pmatrix} -1 & -1 \\ -1 & 1 \end{pmatrix},$$
$$M_{B} = \frac{1}{2} \begin{pmatrix} -1 & 1 \\ -1 & -1 \end{pmatrix},$$

$$Y = \frac{1}{2} \begin{pmatrix} 1 \\ 1 \end{pmatrix},$$
$$X_n^{\Pi} = \begin{pmatrix} \xi_n^{\Pi} \\ \eta_n^{\Pi} \end{pmatrix}.$$

Then from (63) and (64) we have:

$$X_{n}^{\Pi} = M_{\Pi(n+1)}X_{n+1}^{\Pi} + Y, \quad n = 0, \dots, P-1, \qquad X_{0}^{\Pi} = \binom{\xi}{\eta}.$$
(68)



Fig. 12. Triangles and quadrature points distribution for P = 2, N = 9.

 Table 1

 Table showing the convergence of the subdivision method to the exact value

P	Semi-analytical value
0	2.850104132017379
1	2.845615828568151
2	2.841283391873457
3	2.839460514466428
4	2.838225797090046
5	2.837714948869154
6	2.837390629062305
7	2.837256027562511
8	2.837172989130881
9	2.837138477096164
10	2.837117472659868
11	2.837108736937710
12	2.837103455224714
13	2.837101257829896
14	2.837099933576150
15	2.837099382544410
16	2.837099051002786
17	2.837098913034472
18	2.837098830089292
19	2.837098795570917
Exact value	2.837098756400005

We deduce from the previous relation that

$$X_0^{\Pi} = M_n^{\Pi} X_n^{\Pi} + V_n^{\Pi}, \quad n = 0, \dots, P,$$
(69)

where  $(M_n^{\Pi})_{n=0,\dots,P}$  and  $(V_n^{\Pi})_{n=0,\dots,P}$  are two sequences defined by:

$$M_{n+1}^{\Pi} = M_n^{\Pi} M_{\Pi(n+1)}, \quad n = 0, \dots, P-1, \qquad M_0^{\Pi} = \begin{pmatrix} 1 & 0\\ 0 & 1 \end{pmatrix},$$
(70)

and

$$V_{n+1}^{\Pi} = M_n^{\Pi} Y + V_n^{\Pi}, \quad n = 0, \dots, P-1, \qquad V_0^{\Pi} = \begin{pmatrix} 0\\0 \end{pmatrix}.$$
(71)

Fig. 12 shows the distribution of the triangles and the quadrature points after P = 2 steps of the subdivision method.

# 5.2. Numerical experiment

We present below a numerical experiment showing the efficiency of the subdivision method, where the algorithm presented in the previous subsection has been implemented recursively. We consider the situation given by the Fig. 7 with h = 0 and a = 1. We compare the exact value computed by the expression (45) with



Fig. 13. Evolution of the discrepancy  $\delta$  versus *P*.

SAGH<sub>9</sub> using the method described in the previous section. Table 1 shows the evolution of the value obtained by the semi-analytical method versus P, the number of subdivision steps, with 16 digits of precision. We may check when P increases that the precision increases too. The computed value tends to the exact one. Let us consider the discrepancy  $\delta$  defined by:

$$\delta = \frac{|\tilde{K}_P - \tilde{K}_{P-1}|}{\tilde{K}_{P-1}}, \quad P = 1, 2, 3, \dots,$$
(72)

where  $\tilde{K}_P$  is an approximation of  $K_P$  obtained with numerical integration. The Fig. 13 shows the evolution of  $\delta$  versus N. A linear interpolation yields that  $\ln(\delta)$  may be considered as an affine function of P,  $P \ge 2$ , with a good approximation (see Fig. 13).  $\delta < 10^{-q}$ , q being an integer, means that q first digits of the numerical value are stabilized. Thus, although the relative error between  $\tilde{K}_1$  and  $\tilde{K}_0$  is about 0.16%, the graph shows that  $10^{-3} < \delta < 10^{-2}$  meaning the two first digits are stabilized, which could not be enough for a given required precision. For P = 19, only eight digits are stabilized. Between each level, the computation time doubles. Extrapolating the relation between  $\delta$  and P, we get that we should have P = 47 to get q = 16digits stabilized, which corresponds to the machine double precision. However, the computation time becomes  $2^{47}$  times the computation time for P = 0.

The computation time depends also on the platforms that are used to perform it and in the algorithmic methods (sequential or parallel computing). A sensitive advantage is that the method does not require mesh subdivision, as the triangle subdivision is included in the integration method. A compromise has to be found between the acceptable computation time and the accuracy required.

# 6. Conclusion

We derived in this paper a method allowing to calculate integrals of the kind  $I_1$  and  $I_2^k$  without numerical singularities. This method requires the exact analytic calculation of double integrals. We have shown the efficiency of the method in removing these numerical singularities.

The developed semi-analytic method is not symmetric for the calculation of  $I_1$ , unlike the Gauss–Hammer quadrature. It depends on the triangle over which the exact integration is performed. The greater is the triangle, the greater is the error for a pure numerical integration with a given number of Gauss–Hammer points. Thus, since the method is hybrid one using a Gauss–Hammer quadrature combined with an exact integration, the exact integration must be done over the largest of the two triangles so as to achieve the best accuracy.

We presented a subdivision method allowing to improve this accuracy without requiring mesh subdivision. This method leads to a compromise between accuracy and calculation time requirements. It gives satisfactory results in the case of the electromagnetic problem which motivated this work.

Finally, we mention that a great part of this work has been done using Maple releases 6.0 to 8.0, aiming to put the different kernels on a form allowing formal integration.

#### References

- [1] A. Bossavit, Electromagnétisme, en vue de la modélisation, Springer-Verlag, 1988.
- [2] A. Bossavit, J.-C. Vérité, The trifou code: Solving the 3-d eddy-current problem using h as state variable, IEEE Trans. Magn. Mag-19 (6) (1983) 2465–2470.
- [3] H. Brass, G. Hämerlin, in: Numerical Integration III Proceedings of the Conference, vol. ISNM 85, Birkhäuser Verlag, 1987.
- [4] P.-A. Chevalier, Un Modèle Mathématique Pour L'Étude Des Courants De Foucault En Dimension, vol. 3, Department of Mathematics, Swiss Federal Institute of Technology, 1989.

- [5] S. Clain, J. Rappaz, M. Swierkosz, R. Touzani, Numerical modeling of induction heating for two-dimensional geometries, M<sup>3</sup>AS 3 (6) (1993) 805–822.
- [6] Pasi Ylä-Oijala, Matti Taskinen, Calculation of CFIE impedance matrix elements with RWG and n × RWG functions, IEEE Trans. Antennas Propagation 51 (8) (2003) 1837–1846.
- [7] Roberto D. Graglia, On the numerical integration of the linear shape functions times the 3-D Green's function or its gradient on a plane triangle, IEEE Trans. Antennas Propagation 41 (10) (1993) 1448–1455.
- [8] Ph.J. Davis, Ph. Rabinowitz, Methods of numerical integration, Computer Science and Applied Mathematics, second ed., Academic Press, 1984.
- [9] T.O. Espelid, A. Genz, Numerical integration recent developments, software and applications, NATO ASI Series C 357 (1992).
- [10] G. Hämerlin, in: Numerical Integration Proceedings of the Conference, vol. ISNM 57, Birkhäuser Verlag, 1981.
- [11] M. Mori, M. Sugihara, The double-exponential transformation in numerical analysis, J. Comput. Appl. Math. 127 (2001) 287– 296.
- [12] J.-C. Nédélec, Computation of eddy currents on a surface in  $\mathbb{R}^3$  by finite element methods, SIAM J. Numer. Anal. 15 (1978) 580–594.
- [13] J. Rappaz, M. Swierkosz, C. Trophime, Un Modèle Mathématique et Numérique pour un Logiciel de Simulation Tridimensionnelle d'Induction Electromagnétique, Department of Mathematics, Swiss Federal Institute of Technology, Internal Report, 1999.
- [14] J.-C. Vérité, Trifou: un code de calcul tridimensionnel des courants de foucault, IEEE Trans. Magn. Mag-23 (3) (1987) 1881–1887.